



Agilent Technologies

Advanced Design System 2002
Mixer DesignGuide

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Agilent Technologies
395 Page Mill Road
Palo Alto, CA 94304 U.S.A.

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Chapter 1: Mixer QuickStart Guide

This Mixer Quickstart Guide will help you get started using the Mixer DesignGuide. For more detailed reference information, refer to [Chapter 2, Mixer DesignGuide Reference](#).

The Mixer DesignGuide is integrated into the Agilent EEsof Advanced Design System. It contains many analysis schematics and data displays that are useful for the design and analysis of RFIC mixers or the application of discrete mixers in RF systems.

Note This manual is written describing and showing access through the cascading menu preference. If you are running the program through the selection dialog box method, the appearance and interface will be slightly different.

Using DesignGuides

All DesignGuides can be accessed in the Schematic window through either cascading menus or dialog boxes. You can configure your preferred method in the Advanced Design System Main window. Select the *DesignGuide* menu.

The commands in this menu are as follows:

DesignGuide Studio Documentation > Developer Studio Documentation is only available on this menu if you have installed the DesignGuide Developer Studio. It brings up the DesignGuide Developer Studio documentation. Another way to access the Developer Studio documentation is by selecting *Help > Topics and Index > DesignGuides > DesignGuide Developer Studio* (from any ADS program window).

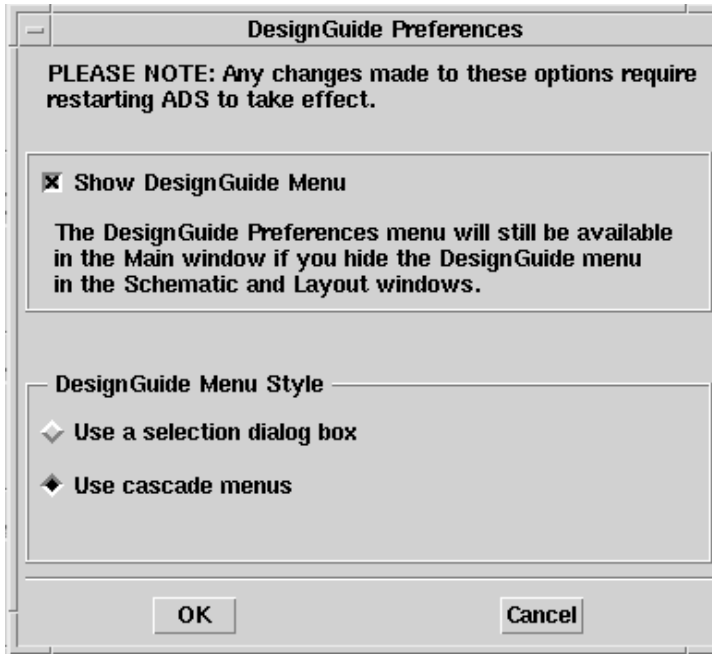
DesignGuide Developer Studio > Start DesignGuide Studio is only available on this menu if you have installed the DesignGuide Developer Studio. It launches the initial Developer Studio dialog box.

Add DesignGuide brings up a directory browser in which you can add a DesignGuide to your installation. This is primarily intended for use with DesignGuides that are custom-built through the Developer Studio.

List/Remove DesignGuide brings up a list of your installed DesignGuides. Select any that you would like to uninstall and choose the *Remove* button.

Preferences brings up a dialog box that allows you to:

- Disable the DesignGuide menu commands (all except Preferences) in the Main window by unchecking this box. In the Schematic and Layout windows, the complete DesignGuide menu and all of its commands will be removed if this box is unchecked.
- Select your preferred interface method (cascading menus vs. dialog boxes).



Close and restart the program for your preference changes to take effect.

Note On PC systems, Windows resource issues might limit the use of cascading menus. When multiple windows are open, your system could become destabilized. Thus the dialog box menu style might be best for these situations.

Accessing the Documentation

To access the documentation for the DesignGuide, select either of the following:

- **DesignGuide > Mixer > Mixer DesignGuide Documentation** (from ADS Schematic window)
- **Help > Topics and Index > DesignGuides > Mixer** (from any ADS program window)

Primary Features of the Mixer DesignGuide

- Passive and active mixer library
- Single-ended and differential Input/Output simulation schematics
- Up or Down conversion
- Sweeps of local oscillator and RF power, LO and RF frequencies, and user-defined parameters

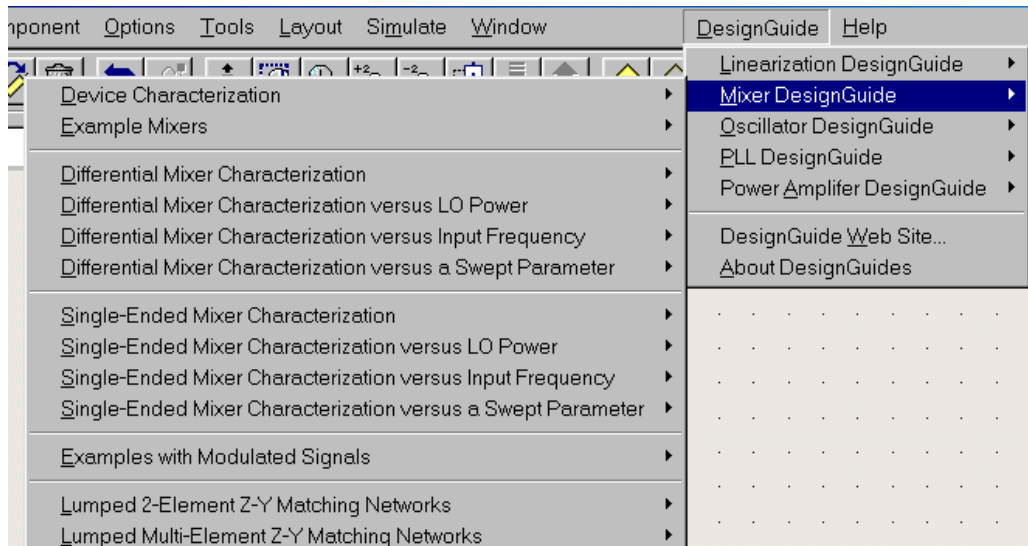
Templates assist in performing the following analyses:

- DC Biasing
- Output spectrum, conversion gain, port impedances, and isolation simulations
- Gain compression
- Intermodulation distortion and intercepts
- Noise figure
- Adjacent channel power with digital modulation

Note The DesignGuide is not a complete solution for mixer and RF system designers, but will provide you with some useful tools. Future versions of this DesignGuide will provide added features. It is intended to save you much time in setting up schematics and display files in particular.

Basic Procedures

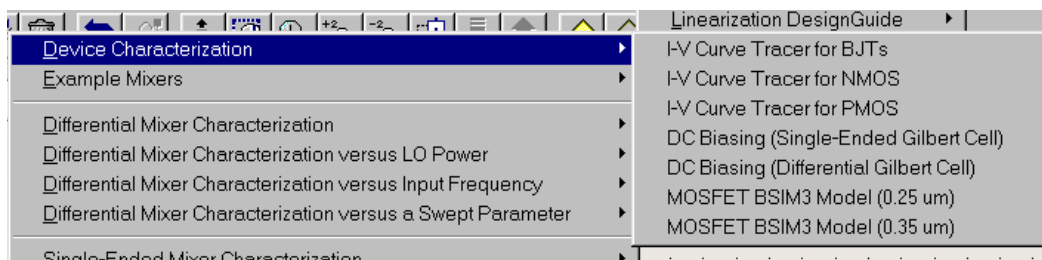
The features and content of the *Mixer DesignGuide* are accessible from the *DesignGuide* menu found in the ADS Schematic or Layout window. Select *Mixer DesignGuide*. A submenu will appear, which lists the various mixer analysis schematics available in this package, as shown in the following figure.



Selecting the Appropriate Simulation Type

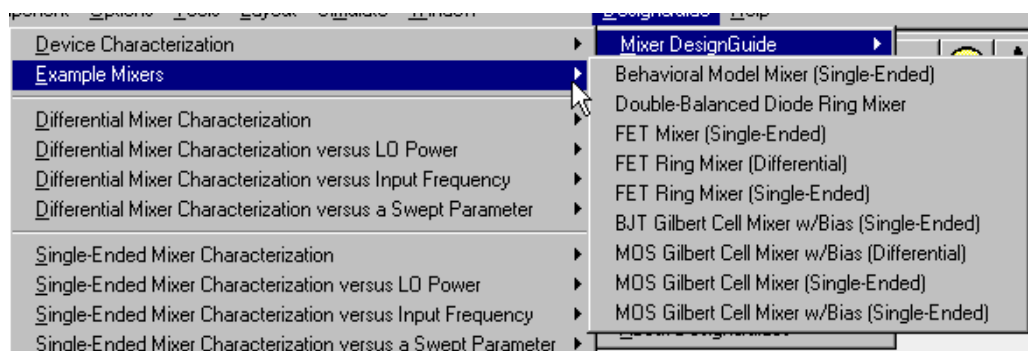
The Mixer DesignGuide has been subdivided into five categories of simulation files that you can use for design and analysis of mixers. These can be seen in the preceding figure.

Device Characterization and Mixer Examples



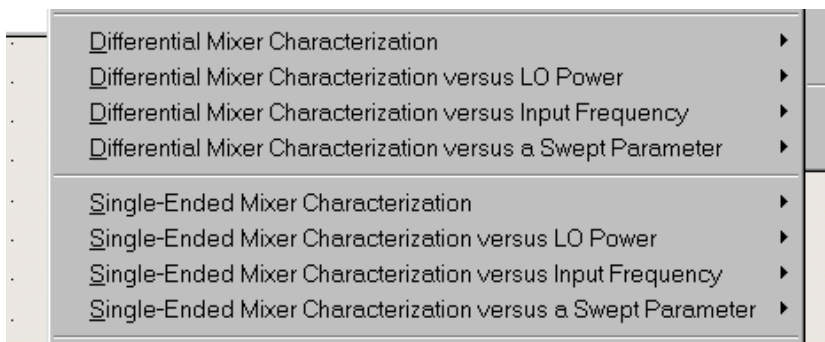
The first menu item provides access to another submenu of curve-tracer schematics for BJTs and MOSFETs shown in the preceding figure. Two sample MOSFET BSIM3 device model parameter sets are also available at the bottom of the menu. Schematics for DC bias point evaluation of active mixer circuits are also available for selection. These can be used when determining the proper DC bias conditions and device widths to be used in a mixer.

A library of example mixers is also available as a starting point for your own design.



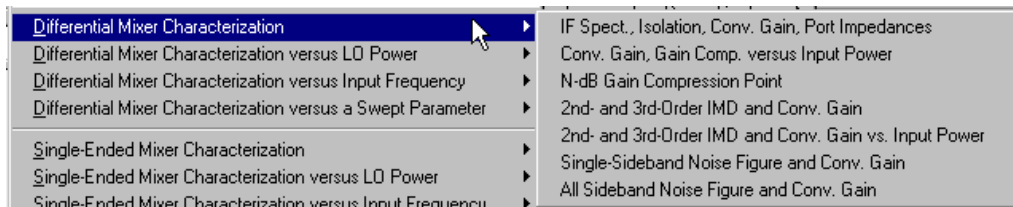
Mixer Characterization

The next two categories are used for evaluation of Differential and Single-Ended Mixer configurations. Characterizations can be selected with no swept parameters, with swept LO power, swept input frequency, or a user-defined arbitrary swept parameter. These options are useful for finding the optimum LO power, bandwidth, and parameters such as device widths or component values respectively.



Each of the four characterization items have identical submenus that can be used to select the type of analysis, as shown in the following figure. When this final selection is made, a schematic with a sample mixer will be copied into your project. Previously simulated results, using the sample mixer, are displayed by the associated data display file that is opened automatically.

To use this simulation tool for your own designs, you must substitute your own mixer schematic into the mixer subnetwork. Push into the subnetwork, delete the existing mixer (but keep the ports), and replace it with your own design. Return to the top-level schematic, set the simulation parameters, and run a simulation. If you keep the top-level schematic name, the corresponding data display will be updated automatically. Also, note that you must provide your own verified nonlinear device models in order to obtain accurate simulation results from these tools.



Tips

- Simulation control parameters that must be set by the user have been enclosed in red boxes on the schematics. An example follows.

VAR
Eqn **R2**

LOfreq=1100 MHz
RFfreq=900 MHz
P_RF=-30
P_LO=0
Zload=400+j*0

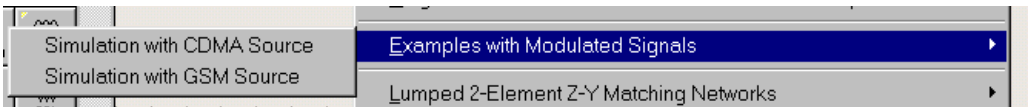
Set the following parameters:

- 1) LO frequency, LOfreq
- 2) Input frequency, RFfreq
- 3) Input power, P_RF
- 4) LO power, P_LO
- 5) Load impedance, Zload

- We have minimized the visibility of equation syntaxes that you should not need to modify.
- Equations that you should not modify have been hidden.
- Note that in all mixer characterization schematics, *RFfreq* is the variable defining the input signal frequency and *IFfreq* is the variable defining the output frequency. If *RFfreq* is higher than *IFfreq*, the simulation is set up for down-conversion. If you want to simulate up-conversion, define *RFfreq* and *IFfreq* such that $IFfreq > RFfreq$.

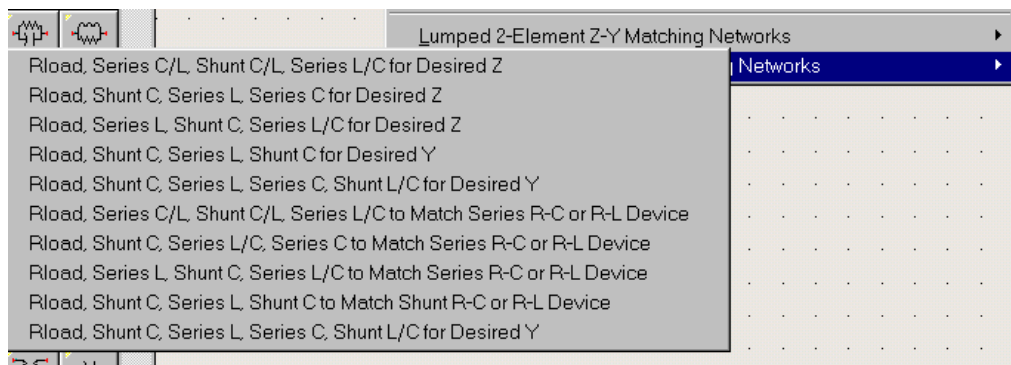
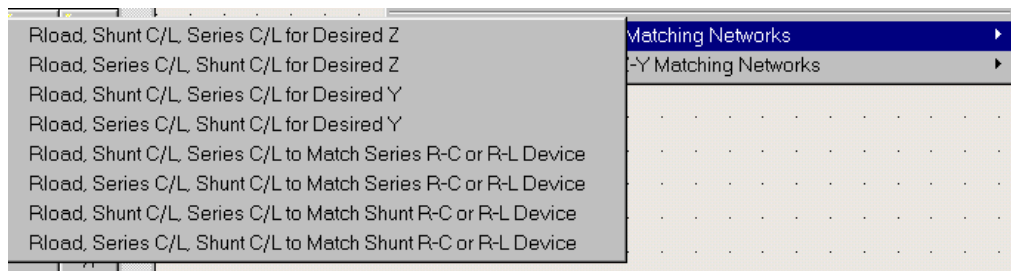
Digital Modulation Examples

Schematics have also been provided for simulation of mixers when driven by digital modulation types such as GSM or CDMA. This is part of the DesignGuide that will be expanded in future versions



Matching Network Design Schematics

You will often find it necessary to design a suitable matching network to interface between stages or to the off-chip (usually 50 ohm) environment. This DesignGuide includes several template schematics that are useful for this purpose when input and output impedances or admittances are known. The S-parameters determined by the schematic called *Mixer Characterization > IF Spect, Isolation, Conv. Gain, Port Impedances* can be used in conjunction with these network design tools to match to a known source or load impedance. Both 2 element and multi-element matching network designs are available.



Note In the ADS product suite, E-Syn can also be used for matching network synthesis.

Chapter 2: Mixer DesignGuide Reference

The Mixer DesignGuide is integrated into the Agilent EEsof Advanced Design System. It contains many analysis schematics and data displays that are useful for the design and analysis of RFIC mixers or the application of discrete mixers in RF systems. The DesignGuide is not a complete solution for mixer and RF system designers, but will provide you with some useful tools. Future versions of this DesignGuide will provide added features. It is intended to save you much time in setting up schematics and displaying files.

Note It is essential that you use verified nonlinear transistor models for the specific process that you will be using to fabricate your mixer. S-parameters are linear small-signal parameters and will not be useful for this purpose. Mixer simulations are very sensitive to the device model because their primary function requires nonlinear operation, either by device nonlinearity or by switching (a large-signal process). Making accurate predictions of gain compression, intermodulation distortion, and calculating intercepts requires models with accurate nonlinearity up to the order of distortion you are simulating.

This DesignGuide provides some generic models for 0.25 μ m and 0.35 μ m NMOS and PMOS FETs and a generic BJT. These models are used in the schematic templates to provide examples of how to use the analysis tools, but will not be valid for your specific design.

Note This manual assumes that you are familiar with all of the basic ADS program operations. For additional information, refer to the ADS User's Guide. For access to the complete set of ADS online documents, select *Help > Topics and Index* from an ADS program window.

Primary Features of the Mixer DesignGuide

- Passive and active mixer library
- Single-ended and differential Input/Output simulation schematics
- Up or Down conversion
- Sweeps of local oscillator power, LO and RF frequency, and user-defined parameters
- Templates assist in performing the following analyses:
 - DC Biasing
 - Output spectrum, conversion gain and isolation simulations
 - Gain compression
 - Intermodulation distortion and intercepts
 - Noise figure
 - Adjacent channel power with digital modulation

Mixer Selection

The Mixer Design Guide is organized according to the choices and steps that are typical for the design and analysis of mixers. First, you will need to decide what type of mixer you are evaluating and whether you will be using it to convert down or up. There are a very large variety of circuit techniques that can provide the mixing operation. If the mixer inputs are at ω_1 and ω_2 , the mixer must provide outputs at $\omega_1+\omega_2$ and $\omega_1-\omega_2$. The mixer will make use of either device characteristics with second-order nonlinearity or modulation of the signal path with a switch driven by the local oscillator to produce these terms.

The best mixers generally are the switching type since they will often lead to fewer spurious outputs (spurs) and can be made to have higher gain compression thresholds. The superior performance is obtained by making sure that the signal path is as linear as possible. This technique is preferred at all frequencies low enough to permit an accurately controlled switching operation. Nonlinear mixers are still used occasionally for millimeter wave applications or noncritical lower frequency uses.

Balancing is also often employed to reduce the number of spurs. Refer to *S. Long, Fundamentals of Mixer Design, Agilent EEsof Design Seminar, 1999* for a description of mixer operation and the important figures of merit associated with mixer performance. (This seminar is provided with your DesignGuide media for your reference.) As shown in [Table 2-1](#), The DesignGuide also provides a sample library of representative mixer types that you can experiment with or modify for your own use.

Table 2-1. Mixer Circuit Library

Mixer Type	I/O	Balance	RF frequency	design file name (.dsn)
Diode ring	Single Ended	Double	wideband	DIODEDB1_mix
MOSFET ring	Single Ended	Double	wideband	FETring_mix
MOSFET ring	Differential	Double	wideband	FETring_Diff_mix
Shunt FET mixer	Single ended	Unbalanced	900 MHz	FET1_mix
MOS Gilbert cell - biased with ideal voltage sources	Single Ended	Double	900 MHz	Gilbert_SE_mix
MOS Gilbert cell - with bias generator	Single Ended	Double	900 MHz	Gilbert_SEbias_mix
MOS Gilbert cell - with bias generator	Differential	Double	wideband	Gilbert_Dbias_mix
Behavioral model mixer	Single Ended	Unbalanced	wideband	SE_Mixer
BJT Gilbert Cell	Single Ended	Double	wideband	GilCellMix

You will be able to use the Mixer DesignGuide most efficiently if you understand what it does when you make menu selections. When you make a menu selection, for example, *Mixer DesignGuide > Differential Mixer Characterization > IF Spect., Isolation, Conv. Gain, Port Impedances*, a schematic (in this case, *Mix_Diff_Spect_Iso*) with a sample mixer, *Diff_MixerUnderTest*, and a corresponding data display are copied into your project.

All of the mixer characterization menu picks copy similar schematics with either the differential sample mixer, *Diff_MixerUnderTest*, or the single-ended sample mixer, *SE_MixerUnderTest*. However, before the Mixer DesignGuide copies schematics, subcircuits, or data displays into your project, it checks to see if files with the same

names already exist in your project. Any files that already exist will not be overwritten. You should push into the sample mixer subcircuit, and modify the schematic or paste your mixer schematic into the subcircuit. You will only have to do this once, as all subsequent mixer characterization schematics inserted via menu picks will use the same subcircuit, named *Diff_MixerUnderTest* or *SE_MixerUnderTest*.

Before using the DesignGuide, you should consider the following choices.

1. Choose a mixer type (Active or Passive).

An active mixer is one that can provide power (conversion) gain from RF to IF. The widely used double-balanced XOR (Gilbert or Jones) style of mixer is an example of an active mixer that is provided in the DesignGuide mixer library. A passive mixer is one that can only provide conversion loss. For example, the FET double-balanced ring or diode double-balanced ring mixers are popular examples also included in the library. It is often easier to obtain large gain compression threshold and intercept point with passive mixers.

2. Choose an I/O configuration (Single-ended or Differential).

This is an important design decision. Differential is generally preferred for RFIC applications, as it lends itself to double balancing without the need for passive baluns or transformers. There is also an advantage in rejection of noise coupled through the substrate due to common-mode rejection. However, if the differential interface on-chip is provided by active *baluns*, the gain compression and intermodulation performance are often limited by the single-ended to differential conversion stage at the input to the mixer. The input *balun* is often implemented as the output of a low noise amplifier.

3. Choose an application (Down conversion or Up conversion).

This choice is clearly dictated by your requirements for RF, LO and IF frequencies. Note that in all mixer characterization schematics, *RFfreq* is the variable defining the input signal frequency and *IFfreq* is the variable defining the output frequency. If *RFfreq* is higher than *IFfreq*, the simulation is set up for down conversion. If you want to simulate up conversion, just define *RFfreq* and *IFfreq* such that $IFfreq > RFfreq$.

DC Analysis

A good place to begin designing either active or passive mixers is with the DC characteristics of the transistor. The purpose for the DC analysis is to establish appropriate bias conditions for the device areas or widths needed in your mixer. In the case of active mixers, bias voltages and currents should be selected for the signal path elements that provide for the best tradeoff between linearity, noise figure, and to minimize compression and distortion at large signal levels.

The DC characterization is useful to the extent that it clarifies the range of operating conditions possible without driving the device into the ohmic or cutoff regions. The designer will need to perform additional analyses to determine the optimum conditions for the above performance measures, since these limits can't be predicted solely by DC evaluations. These other parameterized simulations will be described in a later section. In the case of passive mixers, estimates can be made of R_{on} for selected channel widths and V_{GS} drive levels that will guide the initial design.

In this DesignGuide, under the command sequence *DesignGuide > Mixer DesignGuide > Device Characterization*, we have included schematics and displays for simulation of DC I-V characteristics of NMOS, PMOS and BJT devices as shown in [Table 2-2](#). Some generic BSIM3 device models for 0.25 μm and 0.35 μm MOSFETs have also been provided.

Table 2-2. DC Device and Mixer Simulation files

Analysis	Schematic (.dsn)	Display
Evaluate device ID - VDS	NMOS_curve_tracer PMOS_curve_tracer BJT_curve_tracer	NMOS_curve_tracer PMOS_curve_tracer BJT_curve_tracer
Evaluate mixer DC biasing	Mix_SE_DC Mix_Diff_DC	N/A
0.25 μm MOSFET BSIM3 model	mos25	N/A
0.35 μm MOSFET BSIM3 model	mos35	N/A

These curve-tracer like simulations can be used to help select appropriate bias voltages and currents or to select device widths. For example, in [Figure 2-1](#), we can see that a V_{GS} of 1 V or higher is desired in order to obtain close to maximum G_m . Refer to *S. Long, RFIC MOS Gilbert Cell Mixer Design, Agilent EESOF Design Seminar, 1999* for a detailed example that discusses the selection of bias currents and

device sizes in this commonly-used type of active mixer. (This seminar is provided with your DesignGuide media for your reference.)

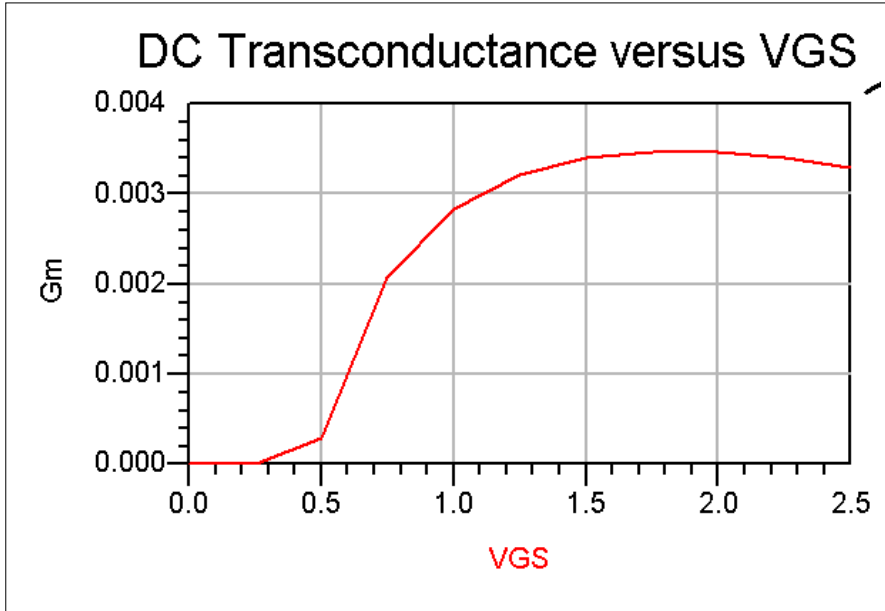


Figure 2-1. DC transconductance versus V_{GS} for a $0.25\mu\text{m} \times 10\mu\text{m}$ NMOS device.

To use the MOS curve tracer schematic (NMOS_curve_tracer or PMOS_curve_tracer) for your design, replace the default device models with your own verified nonlinear device models. Make sure the gate length and width of the model match the parameters L_G and W_1 specified in the VarEqn block shown in Figure 2-2.

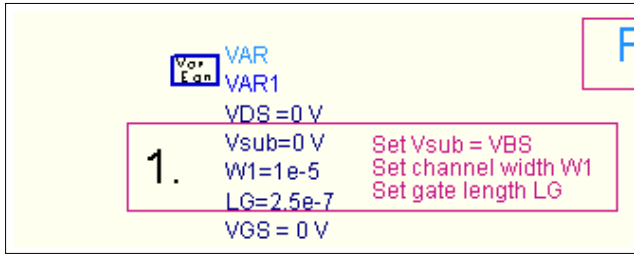


Figure 2-2. Setting bulk-to-substrate voltage, V_{sub} , channel width, W_1 , and gate length, L_G .

Choose the appropriate range for V_{GS} and V_{DS} as shown in Figure 2-3.

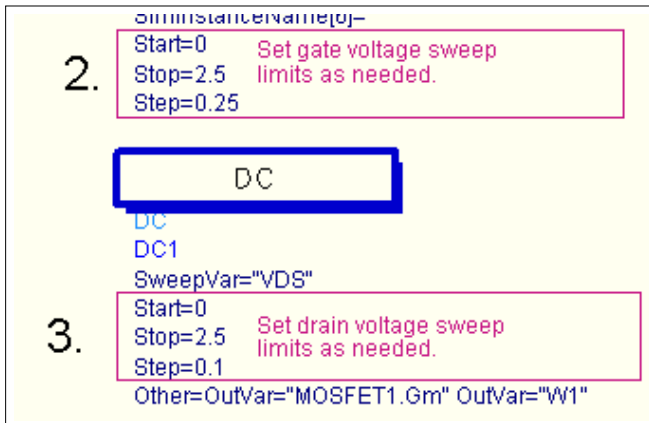


Figure 2-3. Sweep range for V_{GS} and V_D

Two sample schematic files, *Mix_SE_DC* and *Mix_Diff_DC*, have been provided to show how to perform DC simulations of active mixer circuits. You can substitute your own mixer as a subnetwork for the default (Gilbert) mixer used in these examples.

AC Harmonic Balance Analysis

Once the mixer device widths and biasing conditions have been estimated by the dc analysis procedures, you must perform other analyses in order to evaluate and optimize the ac performance. You can follow a sequence of schematics and displays which will lead you through the process of mixer analysis.

Note The schematic and display files associated with these simulations are listed in [Table 2-4](#) through [Table 2-8](#). Note that the filename convention *Mix_XX_Analysis_Parameter* is used throughout this DesignGuide for analysis schematic files. *XX* can represent either Single-Ended (SE) or differential (Diff) I/O. *Analysis* is an abbreviation for the simulation type, and the *Parameter* field is appended when frequency, power, or an arbitrary design parameter is being swept as part of the analysis.

In all mixer characterization schematics, *RFfreq* is the variable defining the input signal frequency and *IFfreq* is the variable defining the output frequency. If *RFfreq* is higher than *IFfreq*, the simulation is set up for down conversion. If you want to simulate up conversion, just define *RFfreq* and *IFfreq* such that $IFfreq > RFfreq$.

Conversion Gain and Gain Compression

The design sequence for passive or active mixers would begin with the evaluation of conversion gain. The theoretical maximum conversion gain is actually a loss for passive mixers: -10 dB for unbalanced or singly-balanced and -4 dB for double balanced designs. For active mixer designs, gain is possible, but must be considered later as a design variable to be traded off against gain compression and intermodulation performance. Several factors will affect the conversion gain including local oscillator (LO) drive level, impedance matching, and device widths.

Each of these should be evaluated to verify that the mixer is performing with the expected gain level. Parametric sweep templates are provided for this purpose. For example, if the LO drive level is too low, the switching devices may switch to the *on* state but have too much series resistance. This will increase the loss and will also affect the large signal performance.

A good place to begin the design is by evaluating conversion gain with a LO power sweep. The schematic files *Mix_XX_CG_LOswp* and display files *Mix_XX_CG_LOswp.dds* (accessed by the menu selection *Mixer DesignGuide > Differential Mixer Characterization versus LO Power > Isolation, Conv. Gain, Port Impedances* or the corresponding menu selection for single-ended mixers) can be used for this purpose. Figure 2-4 shows a plot of conversion gain vs. LO power for a representative differential active mixer. You can see that the gain will saturate as the LO drive increases.

A gain compression simulation that includes a LO power sweep should also be performed. Occasionally the gain compression input power level (*PNdB*) will be more sensitive to the LO drive power than the conversion gain, so both should be evaluated. The schematic files *Mix_XX_PNdB_LOswp* (accessed by the menu selection *Mixer DesignGuide > Differential Mixer Characterization versus LO Power > N-dB Gain Compression Point* or the corresponding menu selection for single-ended mixers) will evaluate gain compression and conversion gain (at the compressed level). The LO amplitude should be increased until the 1 dB (or other gain compression level, N, of your choice) and the conversion gain no longer change significantly with further increases in LO power.

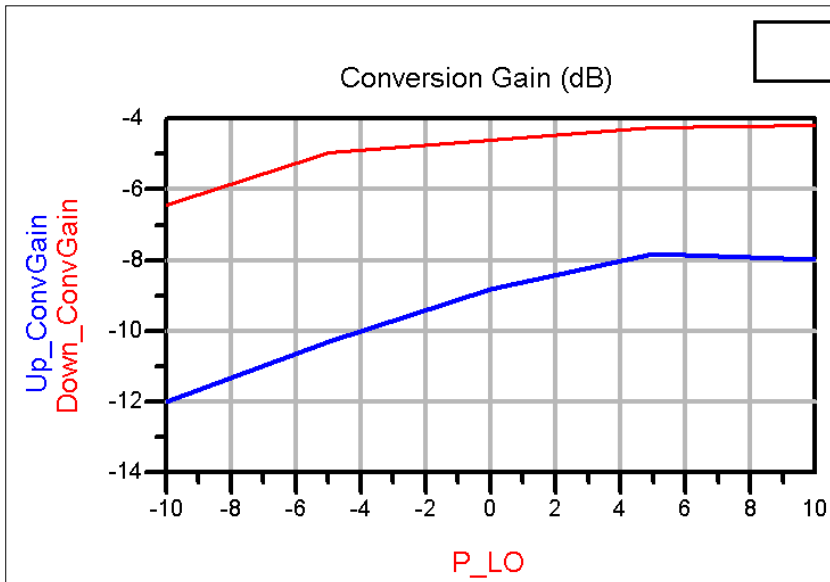


Figure 2-4. Conversion gain as a function of LO power for a differential active mixer from display file *Mix_Diff_CG_LOswp.dds*.

Table 2-3 gives an example of the output of a 1dB gain compression simulation on an active mixer. You can see that the conversion gain is still increasing up to 0 dBm input power but the P1dB input power level has essentially saturated.

Table 2-3. Gain Compression Simulation Result

LO Power dBm	LO voltage @ LOfreq	1.0 dB gain compression input power level (dBm)	Conversion gain
-10	0.188/-20.3	-7.34	-7.70
-5	0.341/-18.0	-7.29	-5.97
0	0.612/-16.1	-7.44	-5.03

Table 2-4 gives mixer design files for gain compression simulations. The menu selections that access these files all end in *N-dB Gain Compression Point*.

Table 2-4. Schematics and displays for N-dB gain compression

Analysis	Schematic	Display
Input power for N dB of gain compression	Mix_SE_PNdB Mix_Diff_PNdB	Mix_SE_PNdB Mix_Diff_PNdB
Input power for N dB of gain compression vs. LO power	Mix_SE_PNdB_LOswp Mix_Diff_PNdB_LOswp	Mix_SE_PNdB_LOswp Mix_Diff_PNdB_LOswp
Input power for N dB of gain compression vs. swept parameter	Mix_SE_PNdB_PRMswp Mix_Diff_PNdB_PRMswp	Mix_SE_PNdB_PRMswp Mix_Diff_PNdB_PRMswp
Input power for N dB of gain compression vs. RF frequency	Mix_SE_PNdB_FRFswp Mix_Diff_PNdB_FRFswp	Mix_SE_PNdB_FRFswp Mix_Diff_PNdB_FRFswp

Mixer Input and Output Matching

Secondly, the design process depends on whether the mixer input and output must be matched to some off-chip impedance source or load, or if the mixer is interconnected on-chip. When needed, matching networks will provide some passive gain and so should be designed before going further with evaluation and optimization of the large-signal performance or noise figure of the mixer. On-chip interconnections should be modeled with appropriate source and load impedances. These may be complex impedances at a single frequency in some cases or if a wider bandwidth design is required, the source and load could be modeled with equivalent circuits.

The *Mix_XX_Spect_Iso*, *Mix_XX_CG_LOswp*, *Mix_XX_CG_FRFswp*, and *Mix_XX_CG_PRMswp* templates also provide the mixer RF and LO input and IF output port impedances and S-parameters. These files are selected by the first menu selection under each of the ...*Mixer Characterization...* menus. This analysis uses the Harmonic Balance simulation method so that these port parameters are measured with the actual large signal LO drive activating the mixer. A small-signal S-parameter simulation could not do this. The parameter sweeps include LO power, RF frequency (with either fixed LO frequency or fixed IF frequency) and a user-defined parameter sweep. Use the *Mix_XX_Spect_Iso.dds*, *Mix_XX_CG_LOswp.dds*, *Mix_XX_CG_FRFswp.dds*, and *Mix_XX_CG_PRMswp.dds* display files that correspond to the schematics above.

Schematic and display file are also provided for the design of two element and multi-element matching networks. These are accessed via the *Lumped 2-Element Z-Y Matching Networks* and *Lumped Multi-Element Z-Y Matching Networks* menu selections. These can work with either admittances or impedances and are useful for narrowband designs.

Spectrum and Isolation

Now that matching network(s), if any, have been added, the mixer IF output and RF input spectra can be viewed using *Mix_XX_Spect_Iso* and *Mix_Spect_Iso.dds*. This can be used with the assistance of markers to identify spurious outputs.

Isolation ratios can also be predicted and displayed with these files and with the same simulation and display files described above for port impedance analysis. The isolation ratio indicates how effectively your mixer will attenuate LO at the RF and IF inputs and RF at the IF output.

Note You should note that very large ratios are sometimes predicted when ideal components are used in balanced mixers. Real components will not be truly identical, and the mismatch in device currents, resistor values, transformer balance, as well as other factors all will degrade the isolation. The sample mixers have been intentionally modified to introduce a realistic amount of unbalance. You will need to do the same for your mixer from your knowledge of the relevant process S-parameter or component variances.

Table 2-5 shows IF spectrum, Conversion Gain, Isolation and Port Impedance Simulations.

Table 2-5. IF spectrum, Conversion Gain, Isolation and Port Impedance Simulations

Analysis	Schematic	Display
Mixer IF and RF spectra; port-to-port isolation; conversion gain, port impedances.	Mix_SE_Spect_Iso Mix_Diff_Spect_Iso	Mix_SE_Spect_Iso Mix_Diff_Spect_Iso
Conversion gain, isolation and port impedances vs. LO power	Mix_SE_CG_LOswp Mix_Diff_CG_LOswp	Mix_SE_CG_LOswp Mix_Diff_CG_LOswp
Conversion gain, isolation and port impedance vs. swept parameter	Mix_SE_CG_PRMswp Mix_Diff_CG_PRMswp	Mix_SE_CG_PRMswp Mix_Diff_CG_PRMswp
Conversion gain, isolation and port impedance vs. RF frequency	Mix_SE_CG_FRFswp Mix_Diff_CG_FRFswp	Mix_SE_CG_FRFswp Mix_Diff_CG_FRFswp

Noise Figure or Large Signal?

Once the correct LO power level is determined and matching networks (if needed) are designed, then you should proceed with both a noise figure and a large signal evaluation. Which one you do first depends on which one of these is most critical for your application. The mixer design approaches for low noise and for large signal handling often are in conflict, so tradeoffs must be made to favor whichever is most critical.

Noise Figure

Two sets of schematic files are available for the mixer noise simulations, one for single sideband NF and the other for “All Sideband” NF. Single sideband noise factor is calculated from the following equation

$$F = \frac{v_n^2 / R_L + kT_0(G_1 + G_2 + G_3 + \dots + G_n)}{kT_0 G_1} \quad (2-1)$$

The single sideband noise figure simulation assumes that the signal input to the mixer is from one RF input frequency only (*RFfreq*). This is normally the case for most mixer applications where an input preselecting filter is applied. In the equation above, the output noise power from the mixer, v_n^2 / R_L , is added to the input noise power kT_0 multiplied by the transducer gains at both mixer input images (G_1 and G_2)

The range of parameters to be swept is entered into the schematic *Mix_Diff_SSBNF_PRMswp* as shown in [Figure 2-6](#).

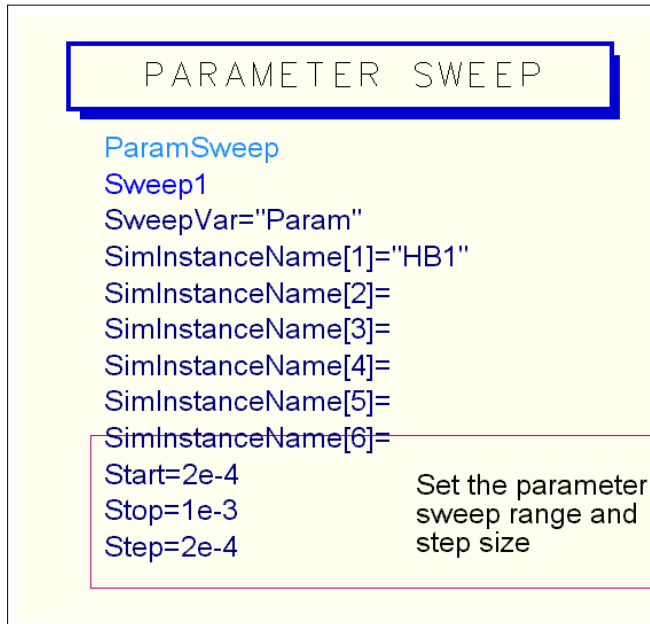


Figure 2-6. Defining the parameter to be swept in the schematic and the parameter sweep range.

As width $W1$ is swept, we see a minimum in noise figure at a width of about $800\ \mu\text{m}$ in Figure 2-7. This is in approximate agreement with the noise model described in Reference [5]. In the figure, MOSFET width $W1$ is the swept parameter (Param). $W1$ is in units of meters.

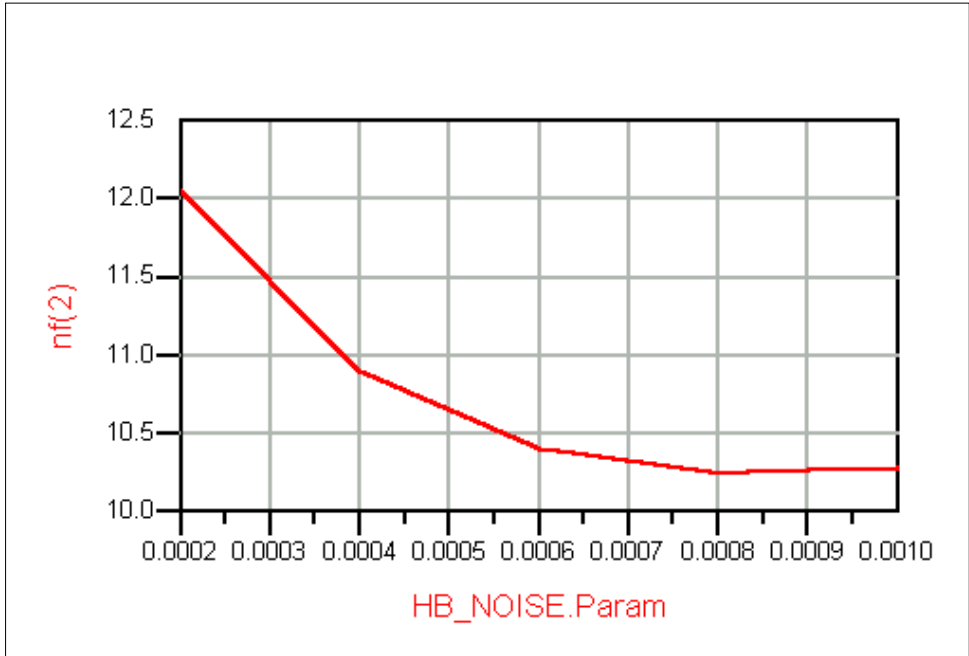


Figure 2-7. Plot of output from *Mix_Diff_SSBNF_PRMswp.dds* display file.

Note This simulated noise figure may not agree exactly with the one that you measure with a hot-cold source noise figure meter by placing a bandpass filter in front of the mixer. This is because the out-of-band mismatch of the filter (S_{11} and $S_{22} = 1$ outside the passband) will reflect any LO or IF components appearing at the mixer input back into the mixer. The remixing that occurs will affect the noise figure in some types of mixers.

The second type of mixer noise figure measurement supported by the DesignGuide schematics is based on the Hot-Cold method referred to above. The schematics (*Mix_XX_HotColdNF*, *Mix_XX_HC_NF_LO_RFswp*, and

Mix_XX_HotColdNF_PRMswp) are configured without any input filters, so a noise figure simulation based on signals at both RF and Image frequencies, and noise at all other LO harmonic images is performed. This is sometimes referred to as the Double-Sideband Noise Figure, but might be more appropriately called the *All-Sideband* noise figure. The noise figure simulated by this method should agree with that measured with a noise figure measurement instrument (assuming the device models for noise are accurate) because it employs the same technique.

A Single Sideband NF can also be obtained by placing a bandpass filter (from the Filters-Bandpass component palette) between the noise source and the mixer RF input. This is similar to the approach that would be used experimentally. However, that this SSB measurement does not provide the NF specified by the IEEE standard [3,4]. Also, the out-of-band reflections will affect the measurement and simulation as described in the preceding note above.

Table 2-6. Design files for noise figure simulations.

Analysis	Schematic (.dsn)	Display
Single sideband noise figure	Mix_SE_SSBNF Mix_Diff_SSBNF	Mix_SE_SSBNF Mix_Diff_SSBNF
Single sideband noise figure with LO power sweep	Mix_SE_SSBNF_LOswp Mix_Diff_SSBNF_LOswp	Mix_SE_SSBNF_LOswp Mix_Diff_SSBNF_LOswp
Single sideband noise figure with parameter sweep	Mix_SE_SSBNF_PRMswp Mix_Diff_SSBNF_PRMswp	Mix_SE_SSBNF_PRMswp Mix_Diff_SSBNF_PRMswp
Single sideband noise figure with RF input frequency sweep	Mix_SE_SSBNF_FRFswp Mix_Diff_SSBNF_FRFswp	Mix_SE_SSBNF_FRFswp Mix_Diff_SSBNF_FRFswp
All sideband noise figure	Mix_SE_HotColdNF Mix_Diff_HotColdNF	Mix_SE_HotColdNF Mix_Diff_HotColdNF
All sideband noise figure with LO power and input frequency sweeps	Mix_SE_HC_NF_LO_RFswp Mix_Diff_HC_NF_LO_RFswp	Mix_SE_HC_NF_LO_RFswp Mix_Diff_HC_NF_LO_RFswp
All sideband noise figure with parameter sweep	Mix_SE_HotColdNF_PRMswp Mix_Diff_HotColdNF_PRMswp	Mix_SE_HotColdNF_PRMswp Mix_Diff_HotColdNF_PRMswp

Large Signal Mixer Simulations

Many applications require the mixer to be free of distortion for rather large input signal levels. Distortion leads to the generation of harmful odd-order intermodulation products (intermodulation distortion or IMD) that can produce spurious signals that may interfere with the desired signal at the IF frequency. Harmonic distortion (HD) also can occur but is usually not a serious interferer as subsequent IF filtering can generally remove it.

This DesignGuide provides two techniques for assessing the large signal performance: gain compression and two-tone IMD simulations. Of the two, the two-tone simulation should provide the most accurate information and gives both second-order-intercept and third-order-intercept as figures of merit. (See the *Fundamentals of Mixer Design* DesignSeminar CD [1] for definitions.)

Gain Compression

Two types of gain compression simulation schematics and displays are provided. First, the *Mix_XX_GC* schematic simulates the conversion gain of a mixer as a function of RF input power. You can set the range of RF input powers. The corresponding display files *Mix_XX_GC* present IF spectra and plots of conversion gain vs. RF input power and IF output power, for both down and up conversion. This simulation allows you to see the details of the gain compression; that is, whether it compresses quickly or slowly as you increase the RF power level at the input.

If you are just interested in finding the input power required for a particular level of gain compression, then the *Mix_XX_PNdB*, *Mix_XX_PNdB_LOswp*, and *Mix_XX_PNdB_PRMswp* schematic files are used to determine this input power for N dB of gain compression. The standard LO and user-defined parameter sweeps are available as usual. Gain compression as a function of input RF frequency can also be simulated for the cases where the LO tracks the RF frequency to give a constant IF output frequency, or for fixed LO and variable IF frequency (*Mix_XX_PNdB_FRFswp*). These simulations have previously been described.

Two-Tone Intermodulation Distortion

A more sensitive way to evaluate the large signal handling capability of a mixer is to apply two or more signals to the input. These dual or multiple signals (tones) mix together and form intermodulation products. Two tone simulations are used in the Mixer DesignGuide to evaluate the IMD generation of your mixer. The results are expressed in terms of the carrier-to-IMD power ratio (dB) and calculated second-

(SOI) and third-order (TOI) intercepts. These results are representative of how well the mixer will perform in a true multicarrier environment. In some cases, you will want to evaluate the mixer's intercept or IMD power as a function of such variables as LO power, DC bias, device widths, resistances or load impedances, and possibly many others.

All of the following simulation files require that you select the RF center frequency ($RFfreq$), LO frequency ($LOfreq$), and a spacing frequency, $Fspacing$, between the two input signals. Thus, the two RF inputs are located at $RFfreq \pm Fspacing/2$. You must also specify the load impedance, $Zload$.

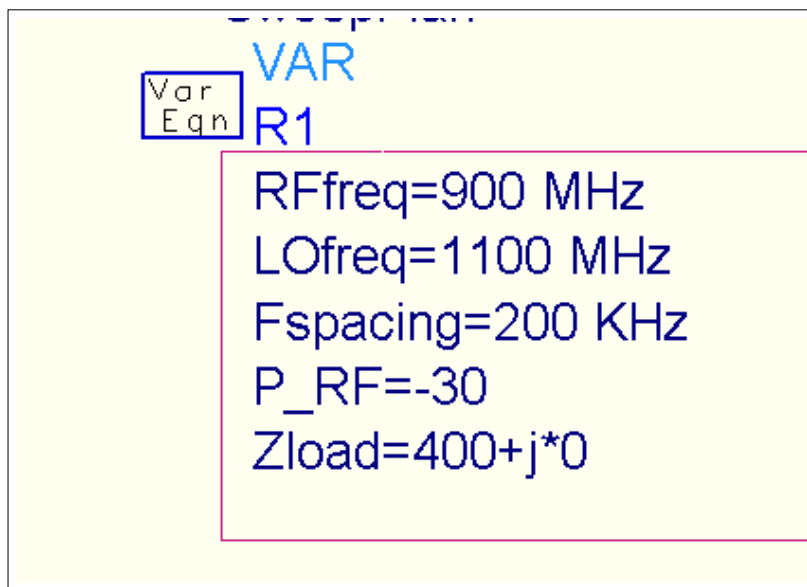


Figure 2-8. Setup for the mixer IMD simulation.

The first simulation template, Mix_XX_TOI , is used to provide a spectral display and to calculate IMD ratio, SOI, and TOI at a fixed RF input power and LO input power. Thus, P_{LO} and P_{RF} must be specified. If your LO source is non-sinusoidal, you may wish to the harmonic amplitudes on the P_nHarm source to higher levels than 100 dB below the fundamental. Harmonics higher than the third may be added, also. You must also specify the Maximum IMD order that you are interested in displaying on the spectral plot. Do not use IMD orders that are much higher than necessary, as it will increase the computation time and data file size. A single display file shows the

results for both up and down conversion. Close-ups of the IF output spectrum at both the up- and down-conversion frequencies are shown automatically as in Figure 2-9. The display zooms automatically to the region close to the designated IF output frequency.

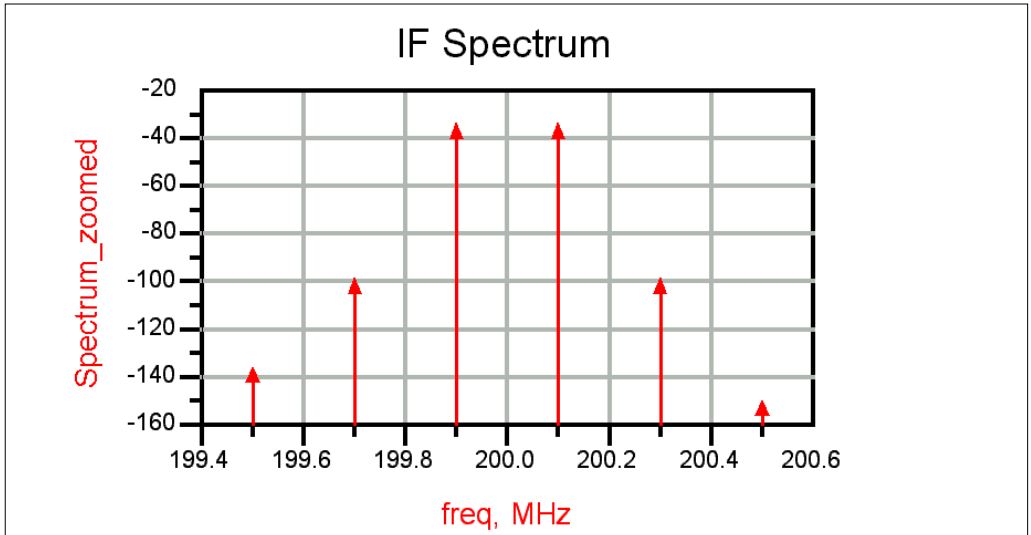


Figure 2-9. Zoomed spectral display of IMD power output from the mixer for fixed RF and LO power levels.

This simulation will provide essentially one data point - projected performance from a single RF input power level. To determine how ideally the mixer is performing, and thus find out if the intercept calculations are valid, you must sweep the RF power and determine if the slope of the third order IMD power is close to 3. Use *Mix_XX_TOI_RFswp* for this purpose. Figure 2-10 shows a plot of the fundamental IF output, *Pout*, and the third-order IMD power as a function of the RF input power per tone.

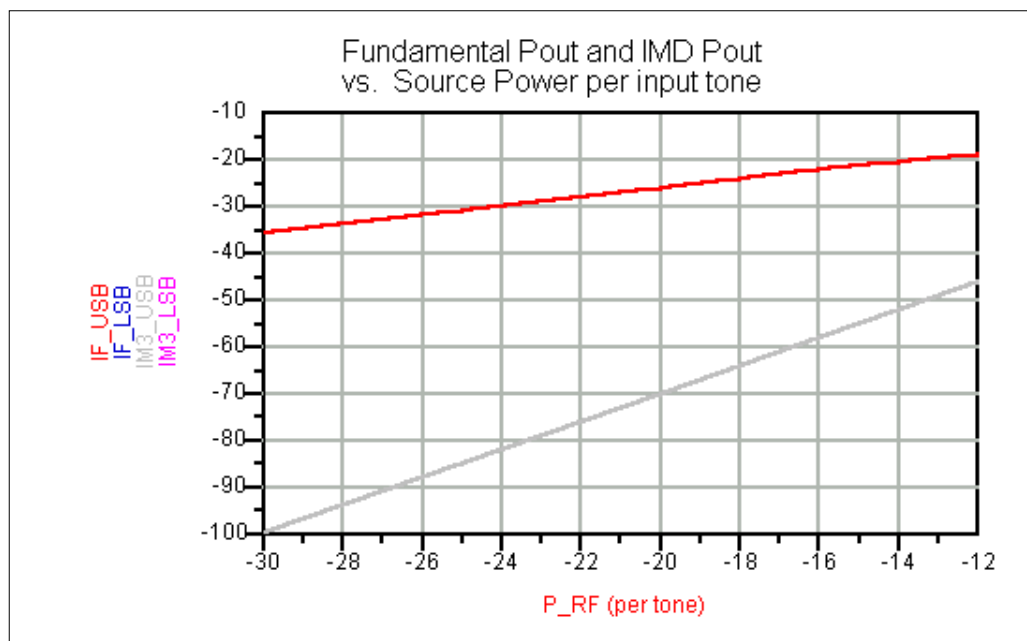


Figure 2-10. Fundamental and IMD output powers from the mixer as a function of RF input power.

Another plot (shown in Figure 2-11) is provided that presents the IF fundamental and IMD slopes vs. P_RF. If the slope is substantially off, you may need to increase the LO order on the harmonic balance controller to improve accuracy. Occasionally, increasing oversampling is also beneficial. The TOI calculation can be performed at any of the swept RF power levels by using the slide marker to set the power level. The calculated TOI will only be valid when the slope is equal to 3.

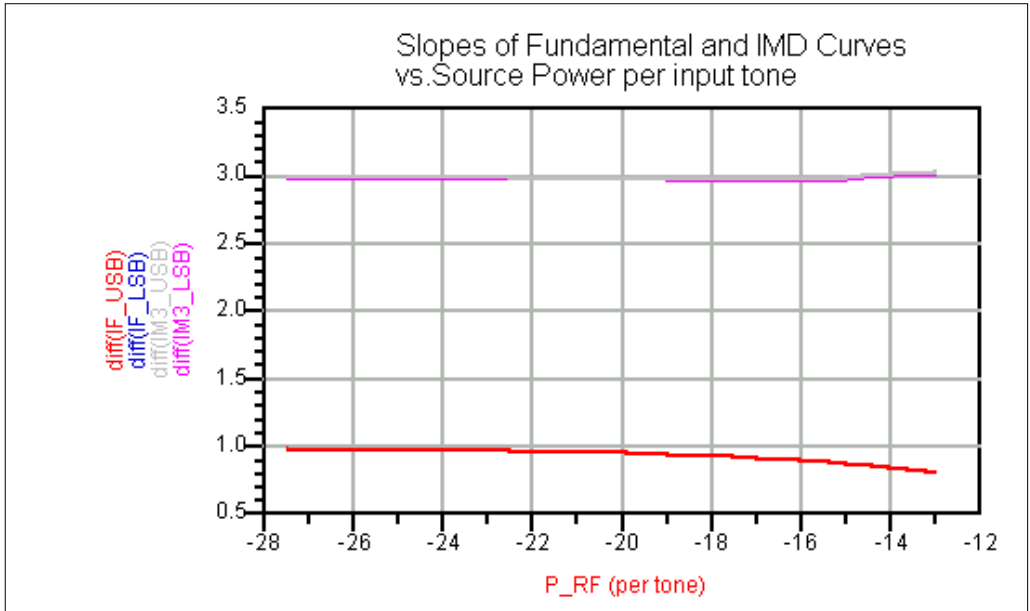
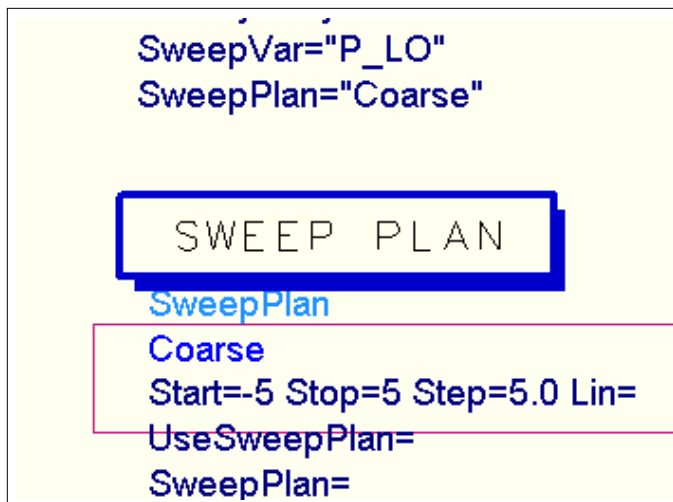


Figure 2-11. Slope of the fundamental and IMD power outputs from the mixer as a function of RF input power per tone.

Other two-tone simulation sweeps: (Schematics: *Mix_XX_TOI_LOswp*, *Mix_XX_TOI_PRMswp*, and *Mix_XX_TOI_FRFswp*; Display files that correspond to these schematics have the same names)

TOI simulation files are also provided to sweep the RF input center frequency, *RFfreq*, the LO power, *P_LO*, or an arbitrary parameter, *Param*. In all cases, the range of the swept quantities must be defined as part of a sweep plan as shown in Figure 2-12. The LO sweep and Parameter sweeps are useful for optimizing the mixer IMD performance which may vary with LO power, bias currents, device widths, and load resistances and impedances. The FRF sweep steps the RF input frequency and allows you to plot mixer IMD performance over an input frequency band. Note

that all of these sweeps are at a fixed RF input power, so it is important to determine first that the mixer behaves normally (third-order IMD slope = 3) before using TOI as an optimization criteria. This procedure is described above.



Intermodulation distortion - Third-order intercept calculation - swept parameter	Mix_SE_TOI_PRMswp Mix_Diff_TOI_PRMswp	Mix_SE_TOI_PRMswp Mix_Diff_TOI_PRMswp
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Digital Modulation Tests

While the two-tone evaluation provides guidance on design tradeoffs that will improve mixer IMD performance, it is not sufficient to guarantee that adjacent channel power (ACP) specification will be met when digital modulation or multicarrier signals are present at the mixer input. Thus, Circuit Envelope simulations using digital modulation sources can be used to simulate the output spectrum and measure ACP. Two sources have been provided for illustrations of the technique. Simulations of GSM and CDMA data sources are given in the schematic and display files GSMtest and CDMAtest. An example of the output spectra simulated with the GSM test is shown in [Figure 2-13](#). Note that the circuit envelope simulations can generate very large data files, you should refer to the ADS documentation on this type of simulation. The frequency axis of the plot is centered around the IF output frequency.

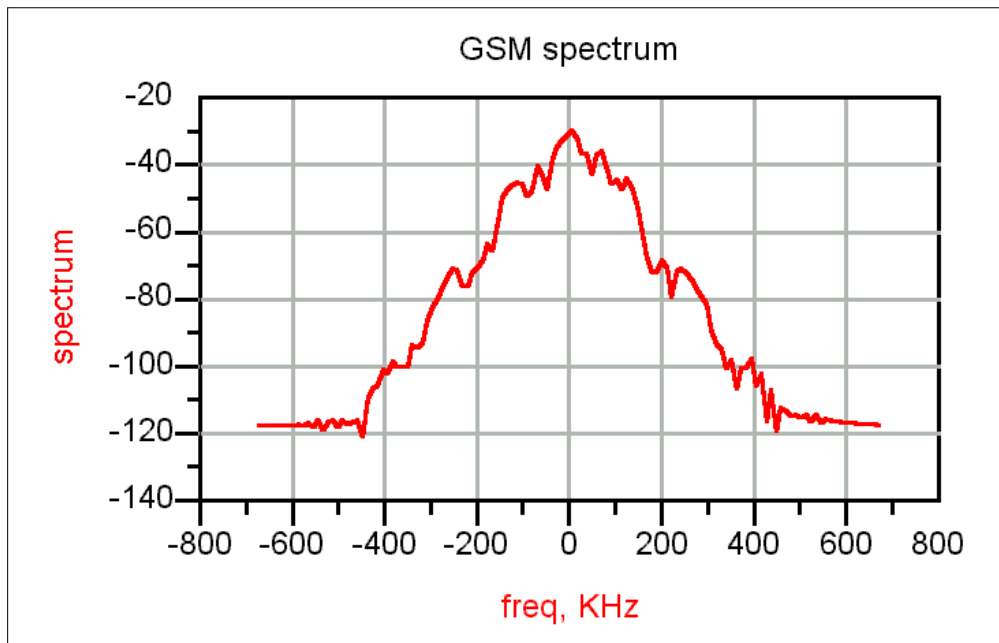


Figure 2-13. Simulated mixer IF output spectrum for a GSM digital signal input.

Table 2-8 shows Circuit envelope simulations for digital modulation.

Table 2-8. Circuit envelope simulations for digital modulation

GSM data source	GSMtest	GSMtest
CDMA data source	CDMAtest	CDMAtest

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